

**CHATSWORTH PRODUCTS, INC.**

**GLOBALFRAME CABINET**

DES. **J. ROBERSON**

JOB NO. **11-1051**

DATE **10/24/12**

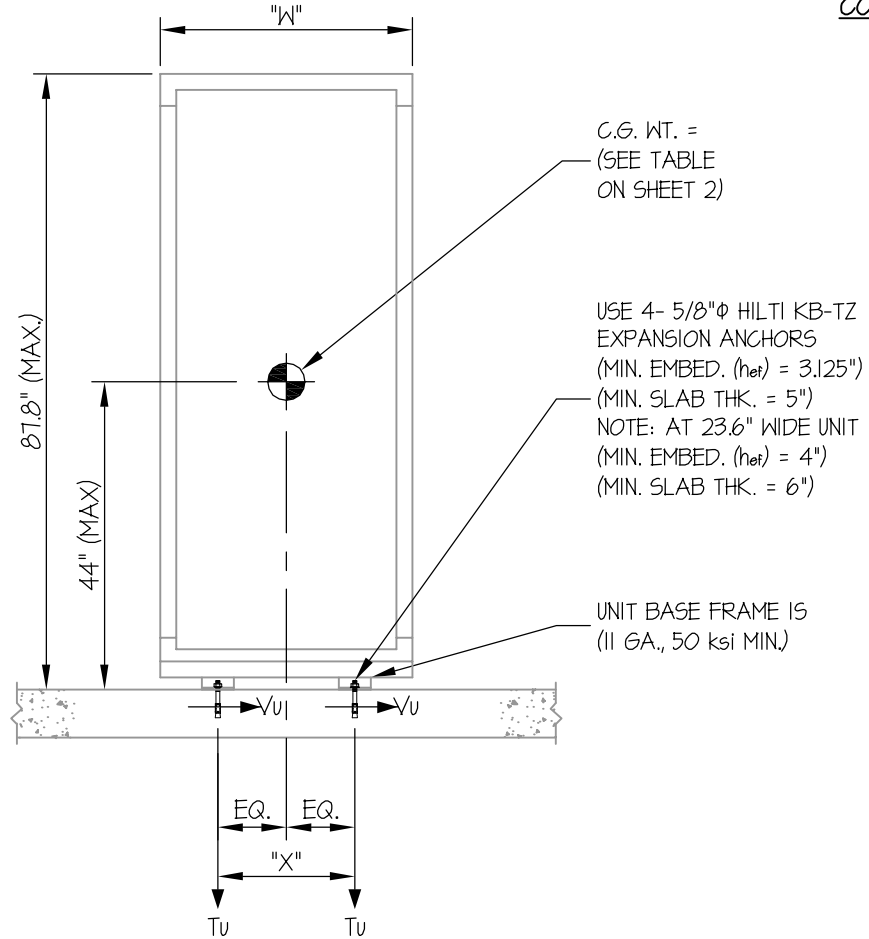
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

CONCRETE SLAB



**FRONT ELEVATION**

NOTES:

1. FORCES ARE DETERMINED PER 2010 CALIFORNIA BUILDING CODE AND ASCE 7-05 STRENGTH DESIGN IS USED.

HORIZONTAL FORCE ( $E_h$ ) =  $0.90 W_p$  ( $S_{ds} = 2.00$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $z/h = 0.0$ )

VERTICAL FORCE ( $E_v$ ) =  $0.40 W_p$

2. CENTER OF GRAVITY (C.G.) WEIGHT IS A MAXIMUM. THIS PRE-APPROVAL ENCOMPASSES ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.

3. STRUCTURAL ENGINEER OF RECORD SHALL PROVIDE SUPPORT STRUCTURE TO SUPPORT WEIGHTS AND FORCES SHOWN.



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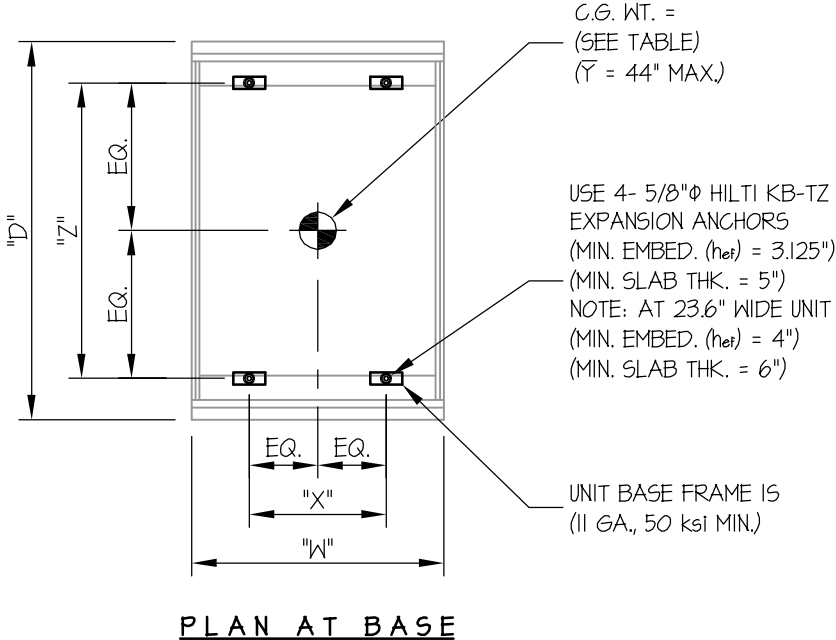
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

CONCRETE SLAB



	WEIGHT (LBS.)	"W" (IN.)	"D" (IN.)	"X" (IN.)	"Z" (IN.)	T <sub>MAX</sub> (LBS.)	V <sub>MAX</sub> (LBS.)
*+	1292	236	315	9.23	21.2	2972	291
+	1317	236	39.4	9.23	29.1	2929	296
+	1324	236	41.3	9.23	31.0	2928	298
+	1343	236	47.2	9.23	36.9	2929	302
	1325	295	31.5	15.14	21.2	1938	298
	1352	295	39.4	15.14	29.1	1875	304
	1358	295	41.3	15.14	31.0	1866	306
	1378	295	47.2	15.14	36.9	1852	310
	1340	315	31.5	17.11	21.2	1759	302
	1366	315	39.4	17.11	29.1	1689	307
	1373	315	41.3	17.11	31.0	1680	309
	1459	315	47.2	17.11	36.9	1741	328

+ FOR 23.6" WIDE UNIT (MIN. EMBED. ( $h_{ef}$ ) = 4") (MIN. SLAB THK. = 6")

\* THIS UNIT IS USED IN CALCULATION BELOW.

LOADS:

WEIGHT = 1292 LB

HORIZONTAL FORCE ( $E_h$ ) =  $0.90W_p$  = 1163 LB

VERTICAL FORCE ( $E_v$ ) =  $0.40W_p$  = 517 LB

BOLT FORCES:

TENSION (T)

$$T_u \text{ MAXIMUM} = \left[ \frac{1163\#(44")}{2 \text{ BOLTS } (21.2")} \times (0.3) \right] + \frac{1163\#(44")}{2 \text{ BOLTS } (9.23")} - \frac{0.9(1292\#) - 517\#}{4 \text{ BOLTS}} = 2972 \text{ LB/BOLT (MAX)}$$

(HORIZ - FRONT TO BACK)      (HORIZ - SIDE TO SIDE)      (0.9(WEIGHT) -  $E_v$ )

SHEAR (V)

$$V_u \text{ MAXIMUM} = \frac{1163\#}{2 \text{ BOLTS}} = 291 \text{ LB/BOLT (MAX)}$$

UNITY CHECK:

$$\left( \frac{T_u}{\phi T} \right) + \left( \frac{V_u}{\phi V} \right) \leq 1.2 \left( \frac{2972}{3178} \right) + \left( \frac{291}{4940} \right) = 0.99 \leq 1.2 \therefore \text{O.K.}$$

BOLT SPEC: 5/8"  $\phi$  HILTI KB-TZ (3.125"  $h_{ef}$ )

$\phi T = 0.75 \phi N_n = 2485 \text{ LB/BOLT (TENSION)}$

$\phi V = 0.75 \phi V_n = 4940 \text{ LB/BOLT (SHEAR)}$

+ BOLT SPEC: 5/8"  $\phi$  HILTI KB-TZ (4"  $h_{ef}$ )

$\phi T = 0.75 \phi N_n = 3178 \text{ LB/BOLT (TENSION)}$

$\phi V = 0.75 \phi V_n = 4940 \text{ LB/BOLT (SHEAR)}$

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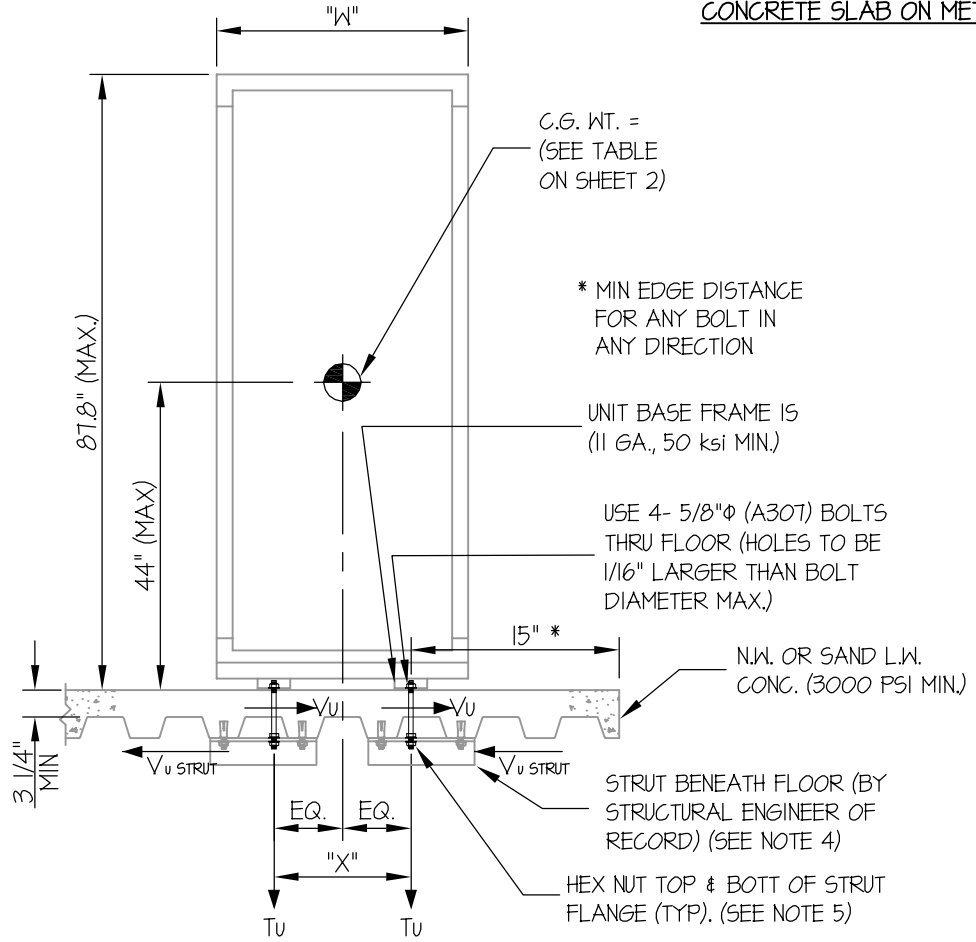
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

CONCRETE SLAB ON METAL DECK



$T_u = 4852 \text{ LB/BOLT (MAX)}$   
 $V_u = 465 \text{ LB/BOLT (MAX)}$

**FRONT ELEVATION**

**NOTES:**

1. FORCES ARE DETERMINED PER 2010 CALIFORNIA BUILDING CODE AND ASCE 7-05 STRENGTH DESIGN IS USED.

HORIZONTAL FORCE ( $E_h$ ) =  $144 W_p$  ( $S_{Ds} = 2.00, a_p = 1.0, I_p = 1.5, R_p = 2.5, z/h \leq 1.0$ )

VERTICAL FORCE ( $E_v$ ) =  $0.40 W_p$

2. CENTER OF GRAVITY (C.G.) WEIGHT IS A MAXIMUM. PRE-APPROVAL ENCOMPASSES ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.

3. STRUCTURAL ENGINEER OF RECORD SHALL PROVIDE STRUCTURE TO SUPPORT WEIGHTS AND FORCES SHOWN.

4. STRUCTURAL ENGINEER OF RECORD SHALL DESIGN THE STRUT(S) AND ITS ATTACHMENTS TO RESIST A LOAD NOT LESS THAN  $V_{u \text{ STRUT}}$  IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT, WHERE  $V_{u \text{ STRUT}} = 0.6V_u \times$  (NO. OF ANCHORS ENGAGED BY STRUT) (MIN)

5. AT CONDITIONS WHERE NUT CANNOT BE PROVIDED AT TOP SIDE OF STRUT, PROVIDE TAPPED HOLE THROUGH STRUT FLANGE.



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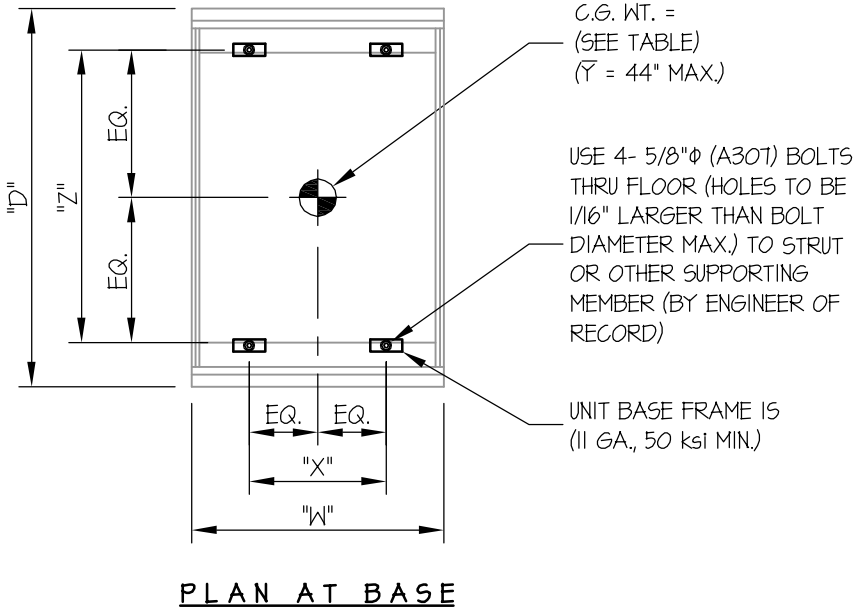
SHEET

**2**

OF **2** SHEETS

SEISMIC ANCHORAGE

CONCRETE SLAB ON METAL DECK



WEIGHT (LB.)	"W" (IN.)	"D" (IN.)	"X" (IN.)	"Z" (IN.)	T <sub>U</sub> (LB.)	V <sub>U</sub> (LB.)
* 1292	236	315	9.23	21.2	4852	465
1317	236	39.4	9.23	29.1	4786	474
1324	236	41.3	9.23	31.0	4785	477
1343	236	47.2	9.23	36.9	4788	483
1325	295	31.5	15.14	21.2	3201	477
1352	295	39.4	15.14	29.1	3102	487
1358	295	41.3	15.14	31.0	3088	489
1378	295	47.2	15.14	36.9	3066	496
1340	315	31.5	17.11	21.2	2914	482
1366	315	39.4	17.11	29.1	2805	492
1373	315	41.3	17.11	31.0	2791	494
1459	315	47.2	17.11	36.9	2895	525

\* THIS UNIT IS USED IN CALCULATION BELOW.

LOADS:

WEIGHT = 1292 LB

HORIZONTAL FORCE (E<sub>h</sub>) = 1.44W<sub>p</sub> = 1860 LB

VERTICAL FORCE (E<sub>v</sub>) = 0.40W<sub>p</sub> = 517 LB

BOLT FORCES:

TENSION (T)

$$T_{U \text{ MAXIMUM}} = \left[ \frac{1860\#(44")}{2 \text{ BOLTS } (21.2")} \times (0.3) \right] + \frac{1860\#(44")}{2 \text{ BOLTS } (9.23")} - \frac{0.9(1292\#) - 517\#}{4 \text{ BOLTS}} = 4852 \text{ LB/BOLT (MAX)}$$

(HORIZ - FRONT TO BACK)      (HORIZ - SIDE TO SIDE)      (0.9(WEIGHT) - E<sub>v</sub>)

SHEAR (V) (ASSUMES HALF THE NUMBER OF BOLTS)

$$V_{U \text{ MAXIMUM}} = \frac{1860\#}{4 \text{ BOLTS}} = 465 \text{ LB/BOLT (MAX) (PER AISC J3.7, LESS THAN 20% STRESS)}$$

BOLT SPEC: 5/8"φ (A36) THREADED ROD

φ<sub>T</sub> = 10,360 LB/BOLT

φ<sub>V</sub> = 5520 LB/BOLT